

近端胃切除人工三角瓣成形抗反流术的力学机理仿真分析

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【摘要】目的:对食管胃结合部腺癌近端胃切除术(PG)人工三角瓣成形后残胃食糜进行流体动力学数值模拟,并计算不同性质胃内食糜的流动特征。**方法:**构建常规PG和人工三角瓣成形术后胃仿真模型,运用Fluent软件对不同粘度胃内食糜反流问题进行数值模拟。**结果:**站立位姿态时,相对常规PG方案,人工三角瓣成形手术方案表现出较好的抗反流作用;卧位姿态时,当胃内食糜粘度大于0.145 2 Pa·s,且胃内食糜不超过人工三角瓣情况下,人工三角瓣成形抗反流手术表现出较好的抗反流效果;人工三角瓣抗反流成形手术方案数值模拟结果与临幊上患者表现一致。**结论:**本研究仿真分析为人工三角瓣成形抗反流手术方案的有效性机理分析、临幊患者术后饮食及手术方案的进一步改进提供理论及数值依据。

【关键词】食管胃结合部腺癌;抗反流;人工三角瓣;计算流体力学

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Simulation analysis on mechanical mechanism of proximal gastrectomy with anti-reflux anastomosis using triangle-valve technique

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Abstract: Objective To carry out the fluid dynamics-based numerical simulation of gastric chyme after proximal gastrectomy with anti-reflux anastomosis using triangle-valve technique (PG-TVT) for the adenocarcinoma of the esophagogastric junction (AEG), and to further analyze the flow characteristics of different gastric chymes. Methods Based on the constructed gastric simulation models after conventional PG or PG-TVT, Fluent software was used to numerically simulate the gastric reflux with different viscosities. Results Compared with conventional PG, PG-TVT had a better anti-reflux effect in standing posture. In supine posture, when the viscosity of the gastric chyme was greater than 0.145 2 Pa·s and the stomach chyme did not exceed the artificial valve, PG-TVT could also achieve a better anti-reflux effect. Moreover, the numerical simulation results of PG-TVT were consistent with the clinical manifestations. Conclusion This simulation analysis provides a theoretical and numerical basis for the analysis on the effectiveness of PG-TVT, the postoperative diet of clinical patients and the further improvement of surgical planning.

Keywords: adenocarcinoma of the esophagogastric junction; anti-reflux; artificial triangular valve; computational fluid dynamics

前言

尽管 Siewert 等^[1]提出了 I~III 型的食管胃结合部腺癌 (Adenocarcinoma of the Esophagogastric Junction, AEG) 分类体系来帮助临幊医生决定手术方式,但 AEG 病例的手术策略仍存在争议。全胃切除术 (Total Gastrectomy, TG) 被认为是一种标准的手术方式,它能切除足够的切缘,是更彻底的淋巴结切除

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术^[2]。最近的一些研究报道,近端胃切除手术(Proximal Gastrectomy, PG)在保留残胃生理功能的同时,其生存率与TG相当^[3-7]。然而,PG术后明显影响患者的生活质量^[8-9]。针对AEG切除手术方案,Gao等^[10]通过临床上的多年经验制定一套全新的人工三角瓣成形抗反流手术方案,该方案已经在临幊上应用多年,效果显著。相比于传统直接切除整个胃或切除胃底的手术方案,该方案是将AEG患者胃底和贲门直接切除,保留胃体和胃窦部分,在胃小弯上通过折叠术形成“三角瓣”一样的膜瓣来阻挡胃内食糜的反流。该手术方案不仅能在人体站立情况下胃消化蠕动时起到抗反流的作用,当人平卧时,折叠术形成的“三角瓣”样式的膜瓣能够在重力作用下贴在胃壁上,起到一定的抗反流效果,这在手术方案上具有突破性的创新。

为了更好地应用并不断优化这类全新的三角瓣成形抗反流手术方案,文章拟从生物力学角度定性、定量的研究其抗反流的力学机制。目前,生物力学在胃功能^[11-15]及相关疾病机理^[16-21]研究中有着广泛的应用。由于胃肠道和消化过程中生物学、生理及神经系统的复杂性,实验往往不能很好地探讨人体胃的混合和消化过程,在体监测不仅昂贵,而且具有局限性,仿真方法则较好地解决了以上问题,因而得

到了学者们的广泛关注。目前,已经出现诸多的数学物理模型和数值模拟方法针对胃内流体混合、胃排空及胃消化功能等问题进行描述和求解^[22-28]。虽然仿真已经运用到胃内各种混合、蠕动及消化的研究中,但是针对抗反流手术后胃内食糜流动的模拟还有所欠缺。

本研究针对常规PG手术成形方案和人工三角瓣成形抗反流手术方案,建立不同手术方案术后胃的三维几何模型,运用计算流体力学Fluent软件模拟患者术后站立和平卧姿态胃内食糜流动过程,比较分析不同粘度的胃内食糜流动特征及不同手术方案抗反流力学机制。为人工三角瓣成形抗反流手术方案的有效性机理分析、临床患者术后饮食及手术方案的进一步改进提供理论及数值依据。

1 材料与方法

1.1 不同手术方案对应的几何模型

根据手术方案运用三维建模软件SolidWorks(美国)分别创建常规PG术后胃模型、人工三角瓣成形抗反流手术后站立姿态胃模型(图1)。人工三角瓣成形抗反流手术后患者处于平卧姿态时,膜瓣在重力作用下会贴于胃壁内侧,如图2所示。



a:常规近端胃切除手术(PG)术后模型



b:人工三角瓣成形抗反流手术术后模型

图1 不同手术方案患者站立时胃几何模型

Figure 1 Geometric models of stomach in standing patients scheduled for different surgical procedures

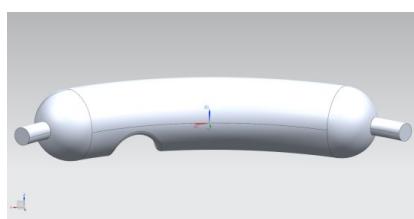


图2 人工三角瓣成形抗反流手术术后患者平卧时胃模型

Figure 2 Stomach model of the patient in supine posture after proximal gastrectomy with anti-reflux anastomosis using triangle-valve technique (PG-TVT)

1.2 胃内食糜物性参数

本文将食糜按粘度大小分成5类(N1~N5),其流体粘度和密度值见表1^[28]。

1.3 网格、控制参数及边界条件设置

由于术后胃形状不规则,采用四面体及六面体

表1 算例中的胃内食糜流体粘度及其密度

Table 1 Fluid viscosity and density of gastric chyme in the calculation example

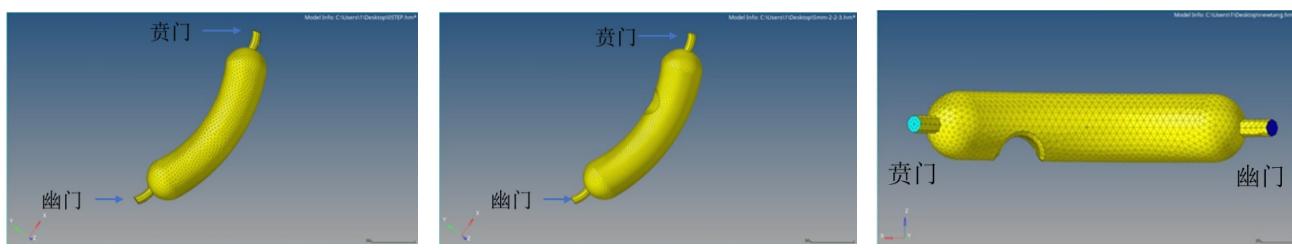
流体	黏度/Pa·s	密度/kg·m ⁻³
N1(水)	0.001	1 000
N2	0.01	1 000
N3	0.1452	1 000
N4	1	1 360
N5(蜂蜜)	10	1 360

混合网格对流场进行离散,其中正常PG术后胃模型离散后网格数为28 869、节点数为5 174。人工三角瓣成形抗反流手术后患者站立姿态模型离散后网格数为44 124、节点数为7 929。人工三角瓣成形抗反流手术后患者平卧姿态胃模型离散后网格数为16 808、节点数为3 093(图3)。胃内食糜均假定为不可压流体,采用SIMPLE方法对问题求解。

求解条件设置如下。(1)流动类型。流动类型设

置为层流。(2)边界条件。幽门入口边界条件:速度入口,速度大小为1 m/s。贲门出口边界条件:outflow出口。壁面条件:无滑移壁面wall。(3)重力加速度。根据术后患者站立时胃的姿态,将重力加速度方向设置为X轴偏Y轴30°,大小为-9.8 m/s²,分解到X轴为-8.486 8 m/s²、Y轴上为-4.9 m/s²。

2 结 果



a:常规PG手术后站立姿态胃模型 b:人工三角瓣成形抗反流手术后站立姿态胃模型 c:人工三角瓣成形抗反流手术后平卧姿态胃模型

图3 不同手术方案术后胃模型网格划分

Figure 3 Mesh generation of gastric models after different surgical procedures

2.1 站立位常规PG手术及人工三角瓣成形抗反流手术后不同粘性流体对比

图4和图5分别是3.5 s时刻常规PG手术和人工三角瓣成形手术后患者胃内食糜流线图。从图4a~图4c可以发现,胃内食糜粘度为0.001、0.01、0.145 2 Pa·s时,胃内幽门入流呈现射流状态射流直接向贲门口喷射,在胃内形成涡流,当胃内食糜达到贲门处时,易形成反流。胃内食糜粘度为1、10 Pa·s时(图4d、图4e),随着胃内容粘度的逐渐增大,由于流体粘滞作用,此时流速较低,射流逐渐消失,胃内涡流也

逐渐消失,当胃内食糜较少时,不易形成反流。

从图5可以观察到,同样粘度条件下,由于人工三角瓣的存在,幽门射流遇到阻挡后,在三角瓣下部区域更易形成胃内涡流,因此,在胃内食糜总量低于人工三角瓣位置时,胃内食糜总量较少,不易形成反流,人工三角瓣成形手术方案对胃内反流具有明显的抑制作用。当胃内食糜粘度较大时(1、10 Pa·s),由于流体粘滞作用,流速较低,胃内涡流逐渐消失,当胃内食糜较少时,不易形成反流。

2.2 平卧位常规PG手术及人工三角瓣成形抗反流手

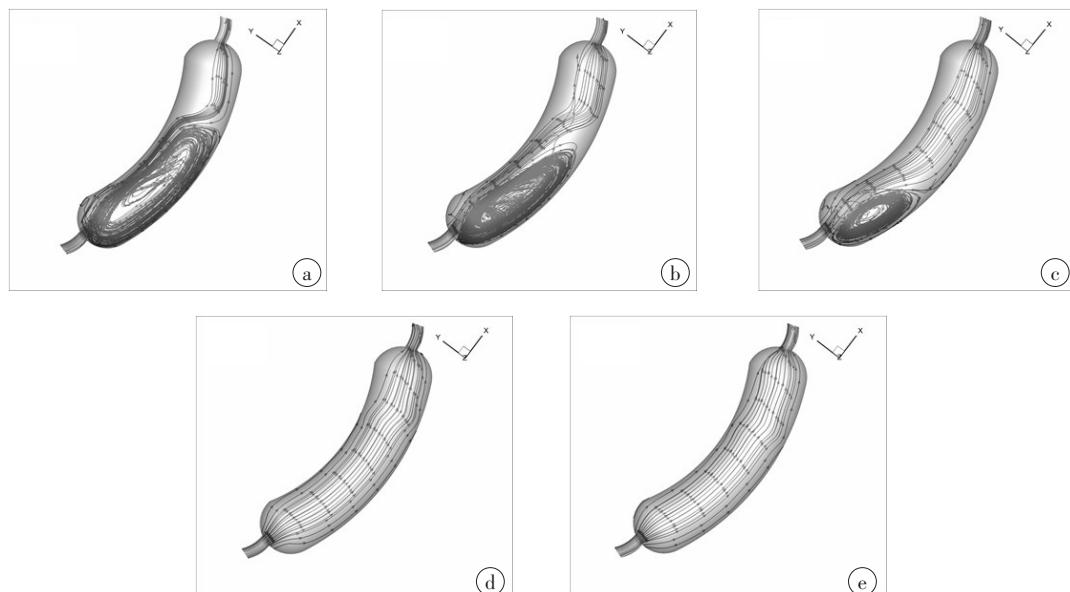


图4 常规PG手术后站立时胃内不同黏度食糜流线图

Figure 4 Streamline diagram of gastric chyme with different viscosities in standing posture after conventional PG

a:0.001 Pa·s;b:0.01 Pa·s;c:0.145 2 Pa·s;d:1 Pa·s;e:10 Pa·s

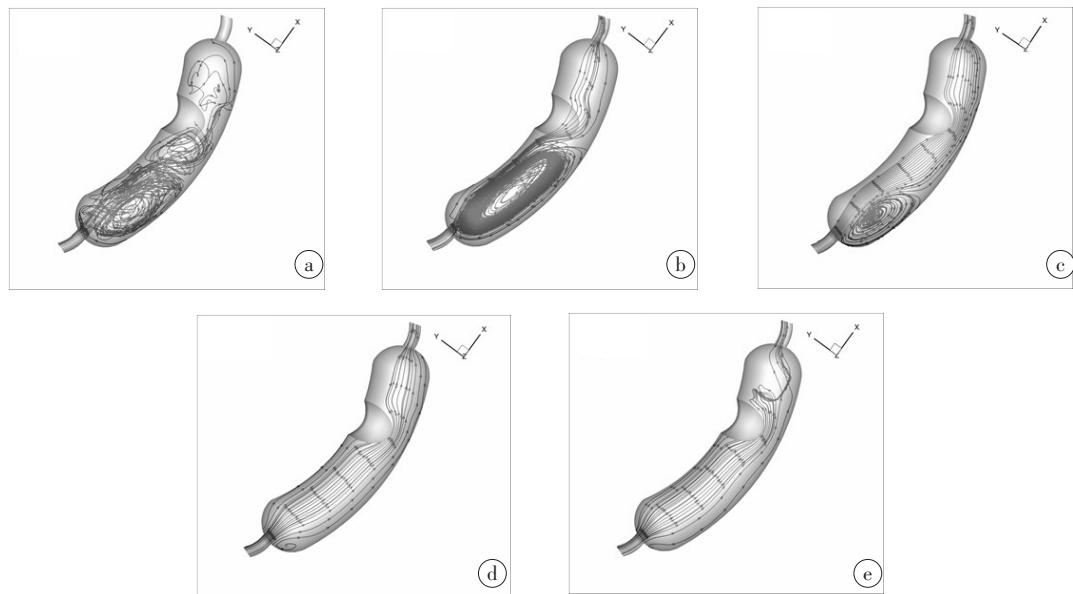


图5 人工三角瓣成形抗反流手术后站立时胃内食糜流线图

Figure 5 Streamline diagram of gastric chyme in standing posure after PG-TVT

a:0.001 Pa·s; b:0.01 Pa·s; c:0.145 2 Pa·s; d:1 Pa·s; e:10 Pa·s

术后不同粘性流体对比

图6与图7分别是0.2、0.3、0.5、1.2、2.2 s时刻常规PG手术及人工三角瓣成形抗反流手术后患者平卧姿态不同粘性胃内食糜与空气分布图,其中右边为幽门入口,左边为贲门出口,蓝色代表胃内食糜,红色代表空气。图8和图9分别是两种手术方案后患者发生反流时对应时刻胃内食糜流线图。从图6和图8可以看出,对于常规PG手术,当胃内食糜粘度为0.001、0.01 Pa·s时,由于胃内食糜粘度低、速度大,常规PG手术后幽门入流形成的射流冲向胃大弯,沿着胃壁直接冲击到

贲门,射流在整个胃腔内形成涡流,易形成反流。当粘度增大(粘度为0.145 2、1、10 Pa·s)时,由于流体的粘滞作用,随着粘度的增大,射流现象减弱,当粘度为0.145 2 Pa·s时,涡流存在于入口处;当粘度为1、10 Pa·s时,胃内部涡流消失。从图7和图9可以看出,对于人工三角瓣成形抗反流手术,当食糜黏度为0.001、0.01 Pa·s时,由于初始速度较大且黏度较小,在惯性力的作用下食糜反流时沿胃壁流动,食糜在三角瓣前方没有聚集。当食糜到达三角瓣时,一部分在三角瓣阻挡下返回到胃体内,在胃体内形成涡流,另一部分食糜越过三角瓣

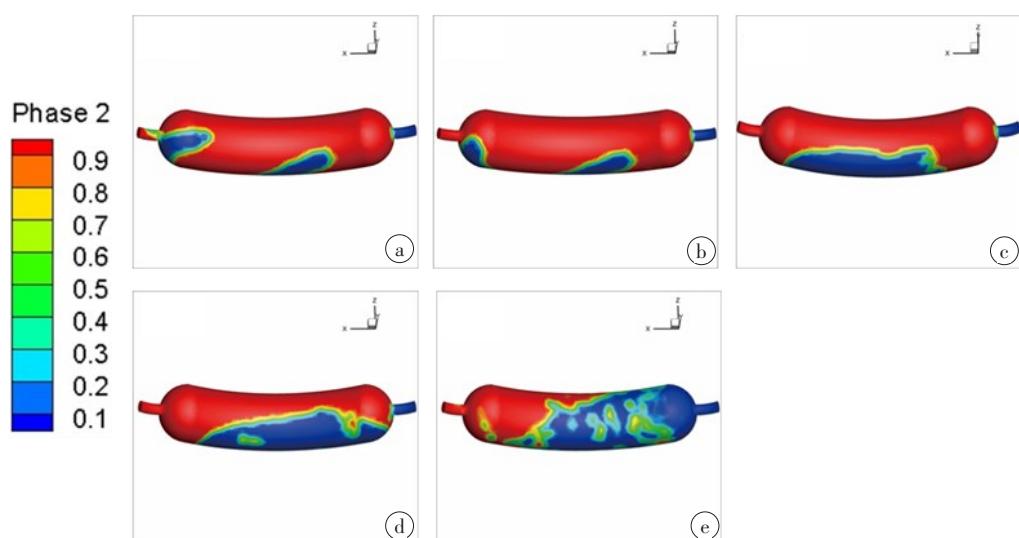


图6 常规PG术后平卧姿态下胃内食糜分布

Figure 6 Distribution of gastric chyme in supine posture after conventional PG

a:0.2 s时刻,0.001 Pa·s;b:0.3 s时刻,0.01 Pa·s;c:0.5 s时刻,0.145 2 Pa·s;d:1.2 s时刻,1 Pa·s;e:2.2 s时刻,10 Pa·s

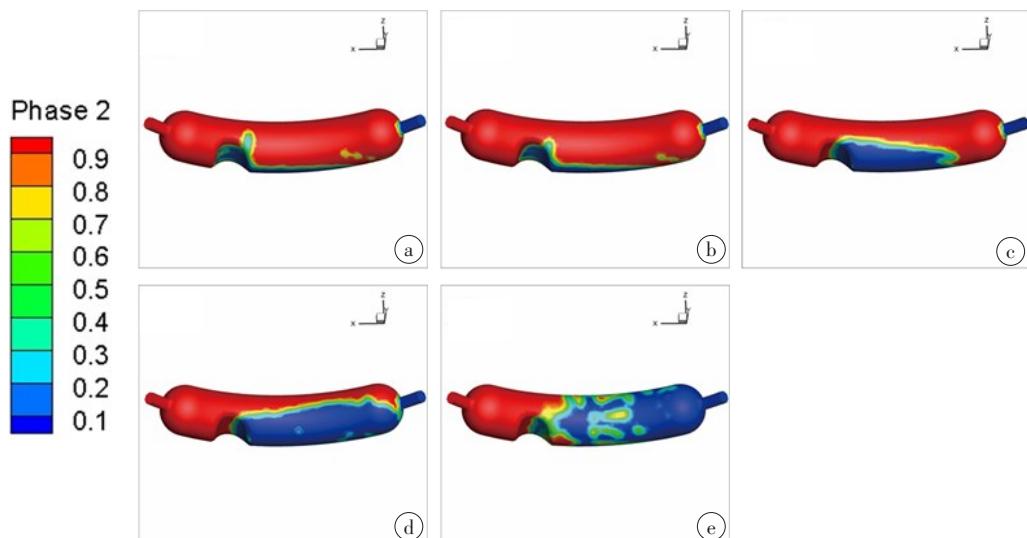


图7 人工三角瓣成形抗反流术后平卧姿态下胃内食糜分布

Figure 7 Distribution of gastric chyme in supine posture after PG-TVT

a:0.2 s时刻,0.001 Pa·s; b:0.3 s时刻,0.01 Pa·s; c:0.5 s时刻,0.145 2 Pa·s; d:1.2 s时刻,1 Pa·s; e:2.2 s时刻,10 Pa·s

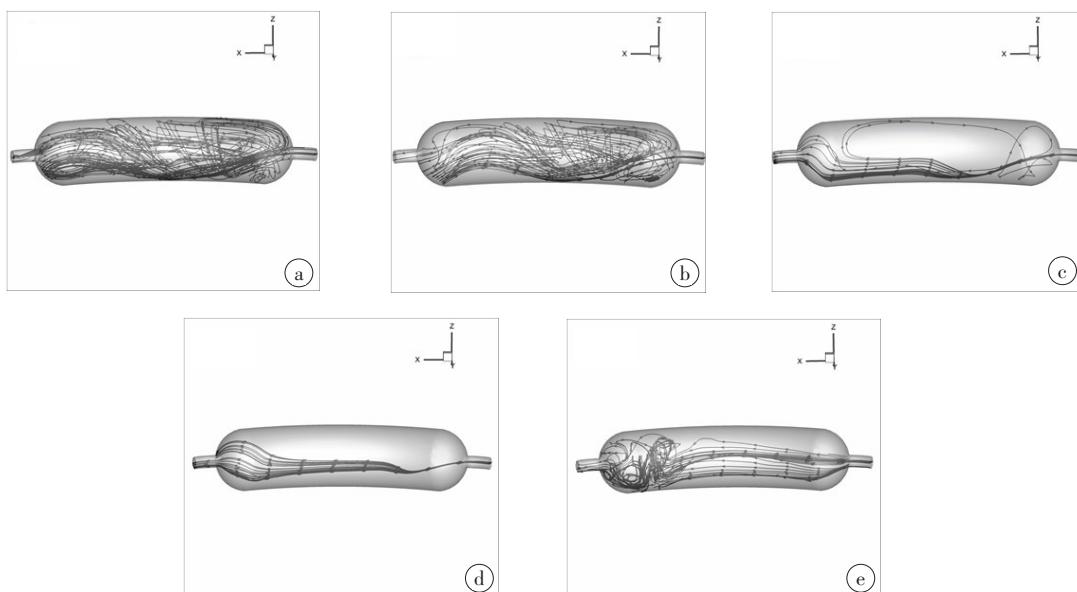


图8 常规PG术后平卧姿态胃内食糜流线图

Figure 8 Streamline diagram of gastric chyme in supine posture after conventional PG

a:0.2 s时刻,0.001 Pa·s; b:0.3 s时刻,0.01 Pa·s; c:0.5 s时刻,0.145 2 Pa·s; d:1.2 s时刻,1 Pa·s; e:2.2 s时刻,10 Pa·s

向贲门流动。当黏度为0.145 2、1、10 Pa·s时,食糜黏滞性增大惯性力逐渐减小,食糜呈均匀流动。当食糜达到三角瓣前方时被阻挡,只有当食糜聚集高度超过三角瓣高度时,食糜才能继续向贲门流动,因此三角瓣起到阻挡作用。

3 讨论

对于AEG,传统的近端胃癌根治手术,患者术后会出现胃食管反流症状,这会明显影响患者的术后生活质量。临床实践表明,PG手术后最常见的问题

是反流,PG手术后100%的患者出现反流症状^[29],发生反流性食管炎的概率为48%^[30]。最近,Masaru等^[31]在使用新型双瓣LPG-DFT技术后没有观察到严重的反流性食管炎,但由于瓣膜成形术复杂,需要熟练地缝合技术,手术时间明显长于TG。本文PG术后人工三角瓣成形抗反流术与传统的全胃切除手术相比有几个优点:手术时间减少、术后营养状况更佳,而且不增加术后相关并发症^[10]。从本研究的结果来看,更进一步证明了该人工三角瓣成形抗反流手术的安全性和可靠性。当手术后患者处于平卧姿态

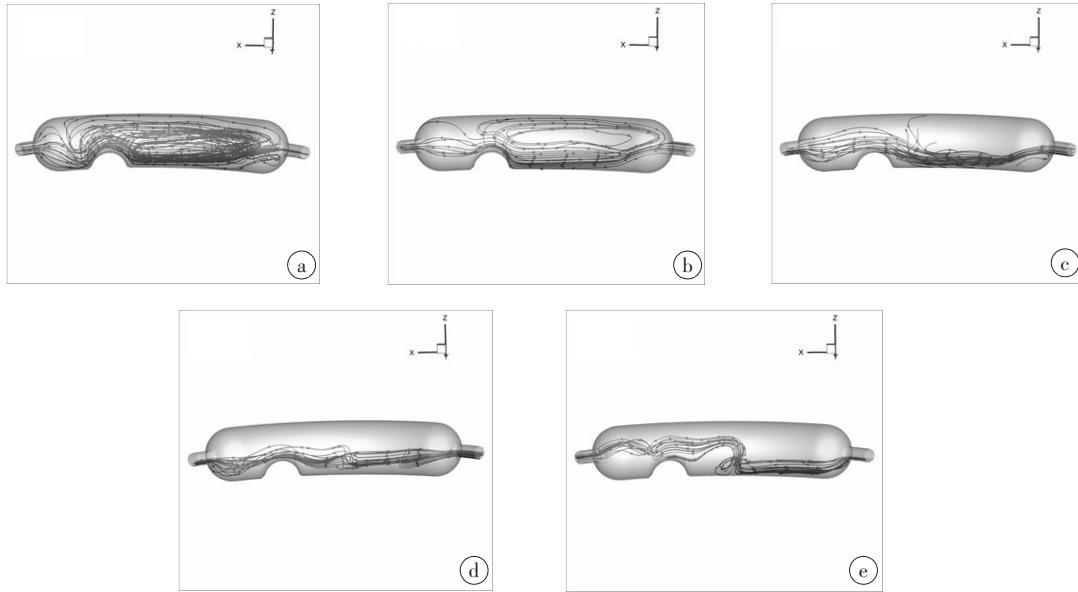


图9 人工三角瓣成形抗反流手术后平卧时胃内食糜流线图

Figure 9 Streamline diagram of gastric chyme in supine posture after PG-TVt

a:0.2 s时刻,0.001 Pa·s; b:0.3 s时刻,0.01 Pa·s; c:0.5 s时刻,0.1452 Pa·s; d:1.2 s时刻,1 Pa·s; e:2.2 s时刻,10 Pa·s

下,胃内食糜粘度较低时,近端胃三角瓣抗反流手术设置的膜瓣并不能很好地起到抗反流的作用,要解决这一问题还需要进一步优化该手术方案。本文下一步的工作是要在现有手术后胃的模型基础上改变该手术三角瓣位置,通过仿真计算对该手术方案的改进提供数值依据。

本文在所构建的常规PG手术成形方案及人工三角瓣成形方案术后患者站立姿态和平卧姿态仿真模型基础上,针对不同粘度胃内食糜反流过程进行了数值模拟。计算结果表明:(1)胃内食糜粘度对其反流过程具有明显的影响作用,无论患者站立或平卧姿态,胃内食糜粘度较大时,胃内食糜流动较为缓慢,不易形成射流,在胃内食糜较少的情况下,难以到达贲门。因此,胃内食糜粘度较大时,不易形成反流。(2)患者站立姿态条件下,当胃内食糜粘度较低时,常规PG手术方案不能很好地抑制射流,射流容易到达贲门。而人工三角瓣成形抗反流方案由于三角瓣阻挡作用,在三角瓣下部更易形成涡流,在胃内食糜较少的情况下,人工三角瓣成形抗反流手术方案表现出较好地抑制反流作用。(3)患者平卧姿态条件下,当胃内食糜粘度较低时,常规PG手术方案由于胃内食糜粘滞性较小,射流速度较大,胃内食糜易沿着胃壁冲向贲门,易形成反流。对于人工三角瓣成形方案,胃内食糜粘度为0.001、0.01 Pa·s条件下,由于较大的惯性力,胃内食糜沿壁面越过三角瓣,人工三角瓣成形抗反流方案抗反流的作用较弱。但当粘度增大(粘度为0.1452、1、10 Pa·s)时,在胃内食糜

较少的情况下,由于三角瓣阻挡作用,人工三角瓣成形抗反流手术方案表现出较好的抑制反流作用。从仿真结果可以看出,人工三角瓣成形抗反流术后患者需控制饮食量,适当增加食物粘度,PG术后人工三角瓣成形抗反流手术效果会更为明显。

本研究通过仿真计算,定量探究了人工三角瓣成形抗反流手术方案术后患者饮食粘度及不同姿态对反流现象的影响,为术后患者饮食及近端胃人工三角瓣成形抗反流方案改进提供了数值依据。

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